

# **Lack Of Penetration in Friction Stir Welds: Effects on Mechanical Properties and NDE Feasibility**

## **AeroMat 2000 Conference and Exposition Friction Stir Joining: Session 4**

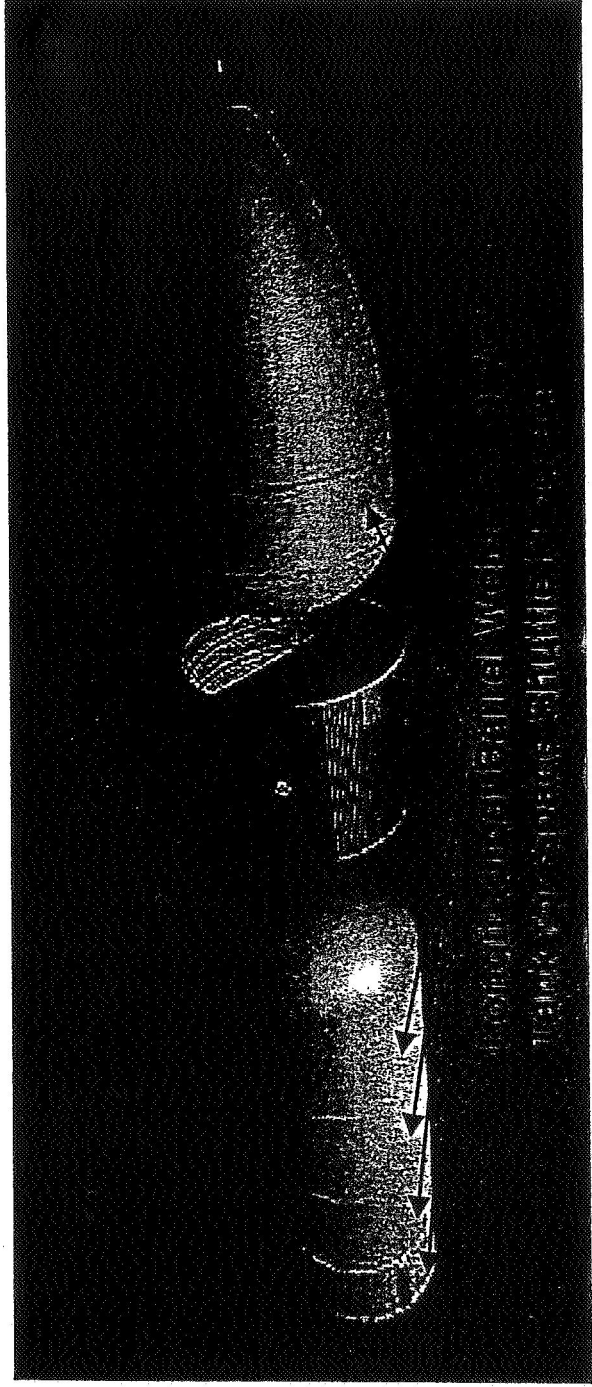
**June 29, 2000**

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Program and Technology Development  
Lockheed Martin Space Systems, Michoud Operations  
New Orleans, LA**

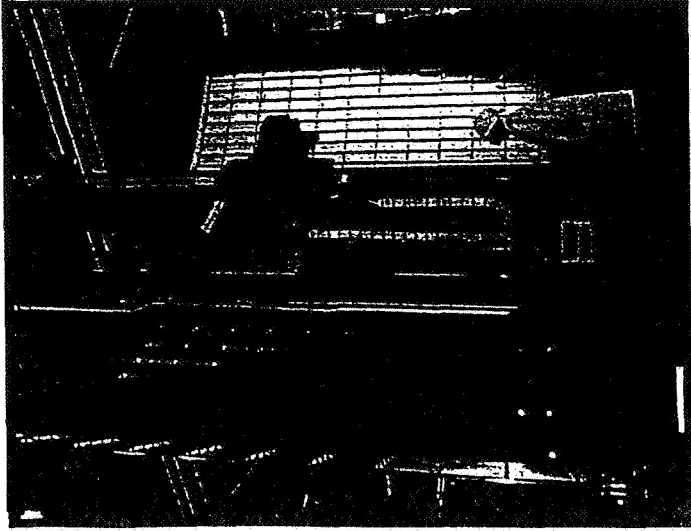
# Acknowledgements and Planned Applications

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- *NASA funded Special Development Studies 1998 and 1999*
  - MSFC Materials and Processes ED33
  - MSFC Welding facility in Bldg. 4705
  - MSFC NDE support
- *LMMSS*
  - M&P Test Laboratories
  - NDE Development Support
- *Outside Contractors*
  - JENTEK Sensors, Inc.
  - Sonic Systems International & Automated Inspection Systems
  - RD/Tech
  - Krautkramer



# Overview of Development Activities

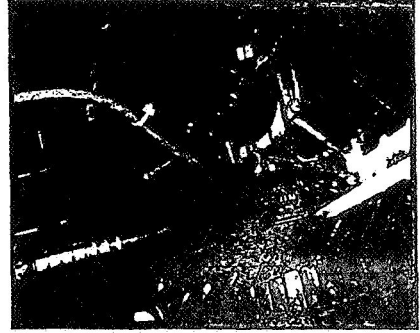
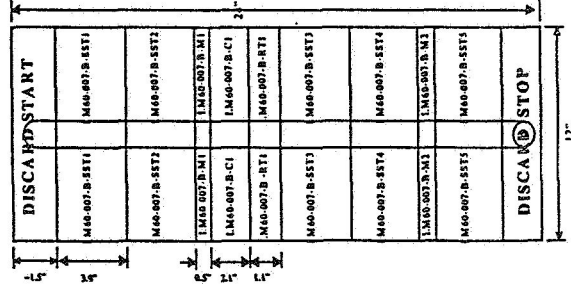


## Vertical FSWelder at MSFC Bldg. 4705

- 0.32" & 0.65" Al 2195T8M4 Plate
- RPM, IPM and plunge force varied during weld development experimental designs
- Confirmation and full scale panels welded
- Demonstration hardware completed

## Square Butt Joint 0.32" & 0.65" Thick

- Al2195 and Bi Metal, Al2219 to Al2195 Joints
- Tapered
- Two-Sided
- Joint Gap
- Repair Methods

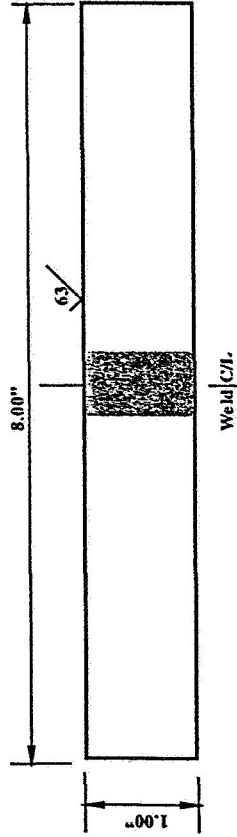


## Mechanical Properties Tests

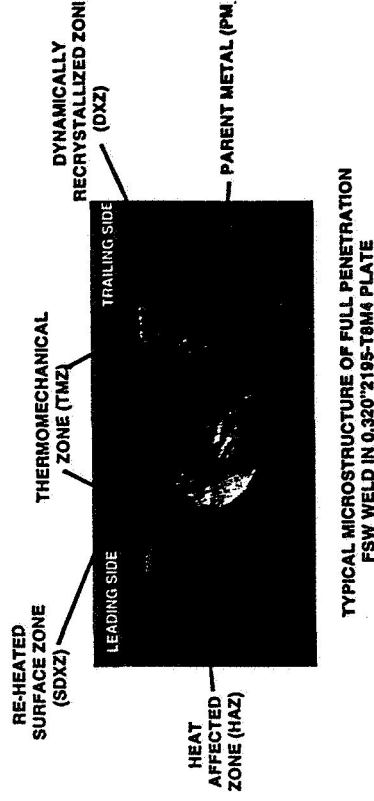
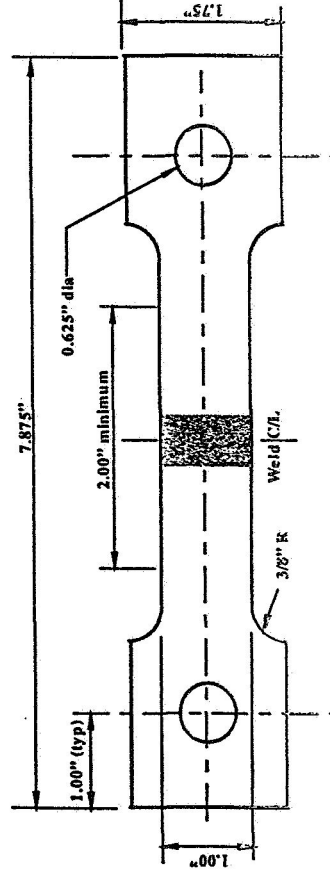
- Tensile, yield and elongation at room, cryogenic and elevated temperatures
- SCT and SST at room, cryogenic and elevated temperatures

# FSWeld Mechanical Properties Specimens & Tests

- Room Temperature Tensile Specimen



- Cryogenic & Elevated Temperature Tensile Specimen



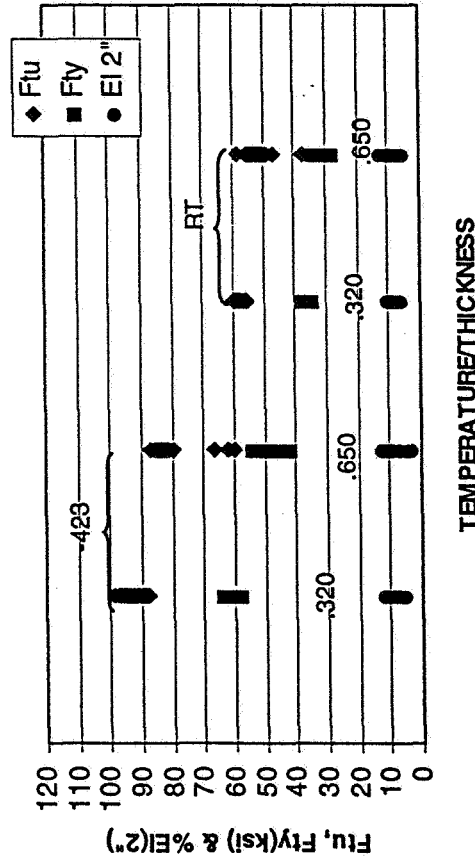
## Test Temperatures

- 423°F
- 320°F
- 70°F
- +200°F
- +300°F



# FSWeld Mechanical Properties Test Results

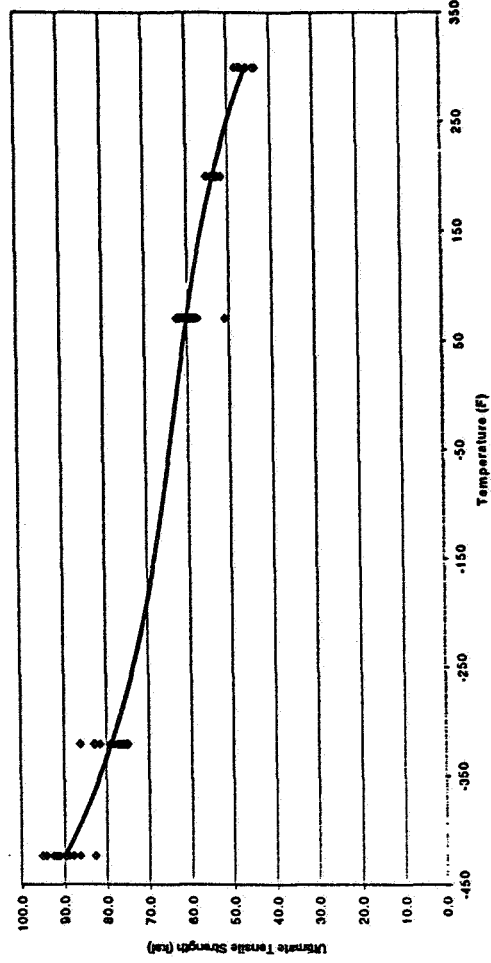
FRICION STIR WELD SDS 3758 DOE ONLY  
.320 & .650 PLATE-TO-PLATE



## 0.320" & 0.650" RT & Cryogenic Tests

- DOE, verification and full-length
- Reduction in strength vs thickness
- Elongation consistent and reproducible

Ultimate Strength vs. Temperature FSWeld Al2195  
0.320" Plate and Extrusion



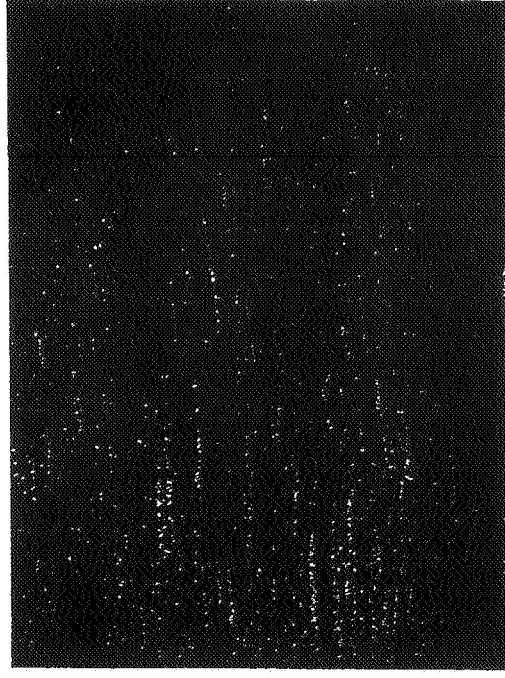
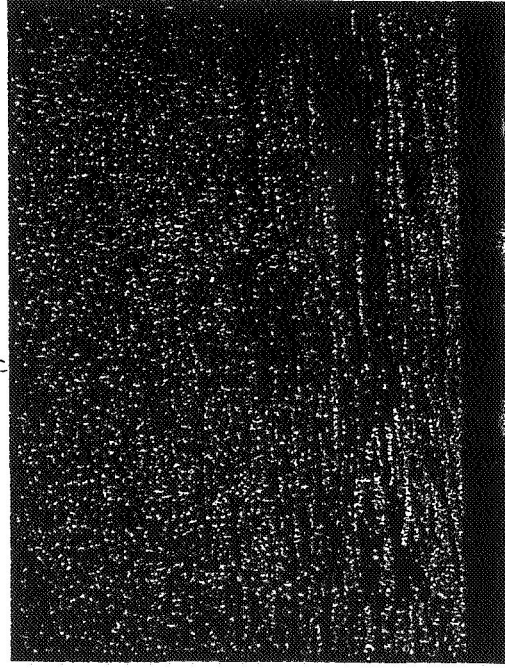
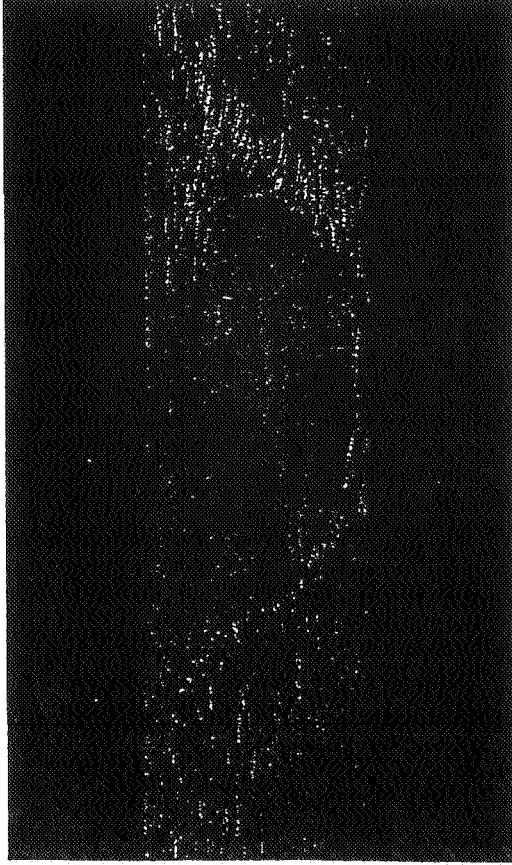
## 0.320" & 0.650" Cryogenic Enhancement in Strength

- 1.5X Ftu and Fty
- Elongation consistent with RT
- Elevated temp, Reduction
- 0.75X Ftu and Fty @ +300F

# FSWeld Lack Of Penetration

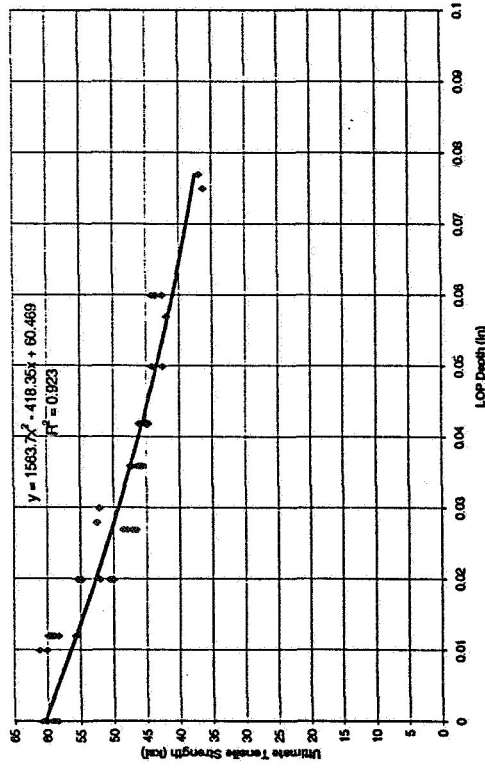
- *LOP - Lack Of Penetration*

- Root Side of Weldment
- Surface Breaking Defect
- Results from incomplete penetration of the DXZ
- Frequently referred to as "kissing bond"
- Requires micro examination to detect
- Range of LOP studied from 0.02 to 0.075"

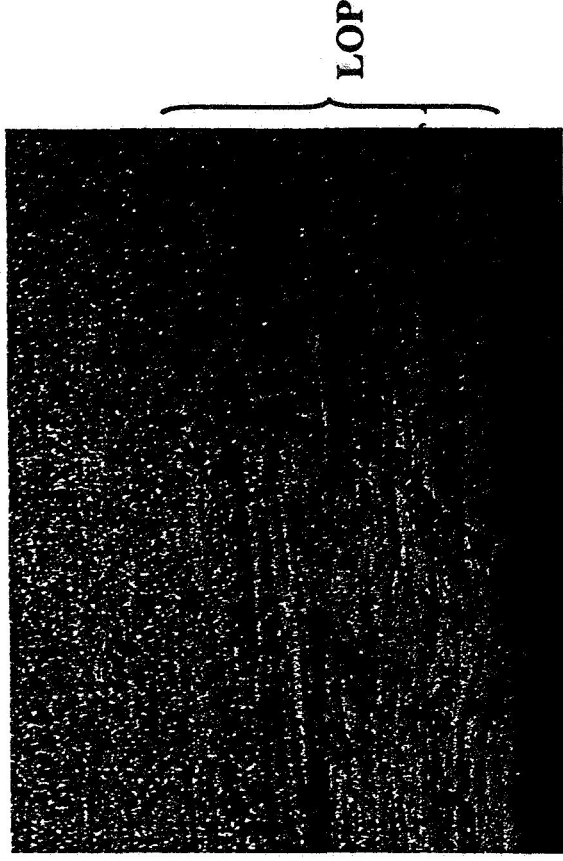
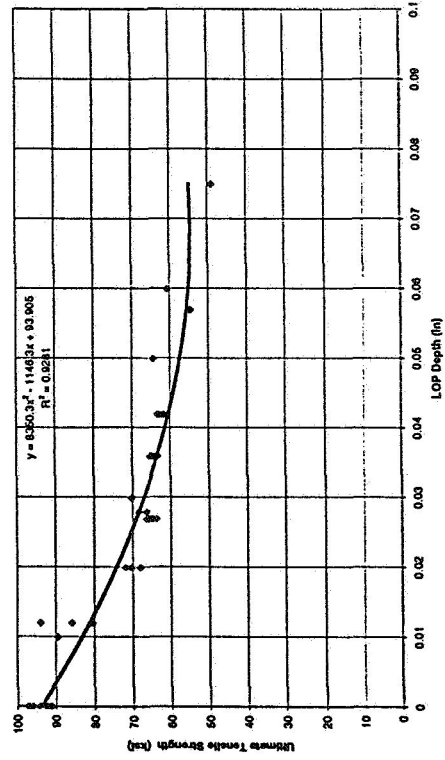


# LOP in FSWeld: Mechanical Properties Results

Ultimate Tensile Strength vs. LOP Depth  
0.32" - 2195 PI to PI at Room Temp



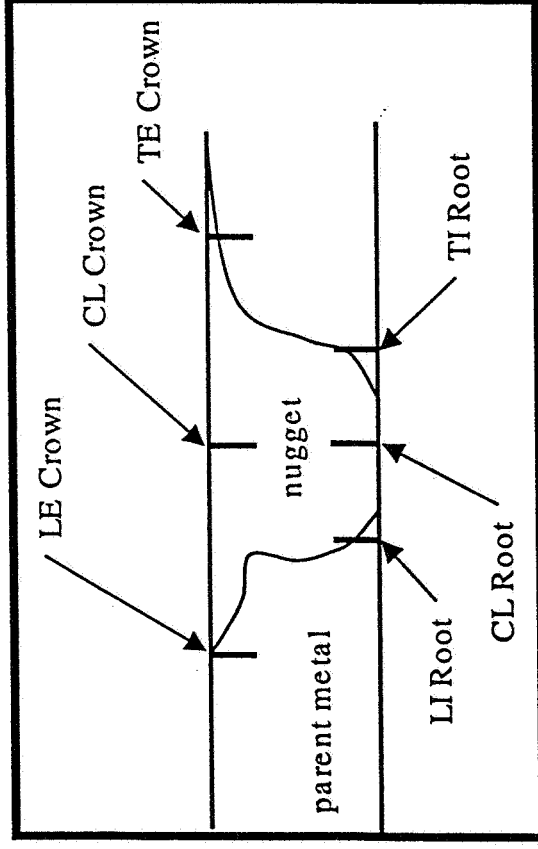
Ultimate Tensile Strength vs. LOP Depth  
0.32" - 2195 PI to PI at -423F



## • LOP - RT and Cryo Tensile Results

- Consistent, repeatable results
- Predictable as a function of LOP depth
- UTS results compared closely to gross fracture stress at ultimate failure after simulated service tests

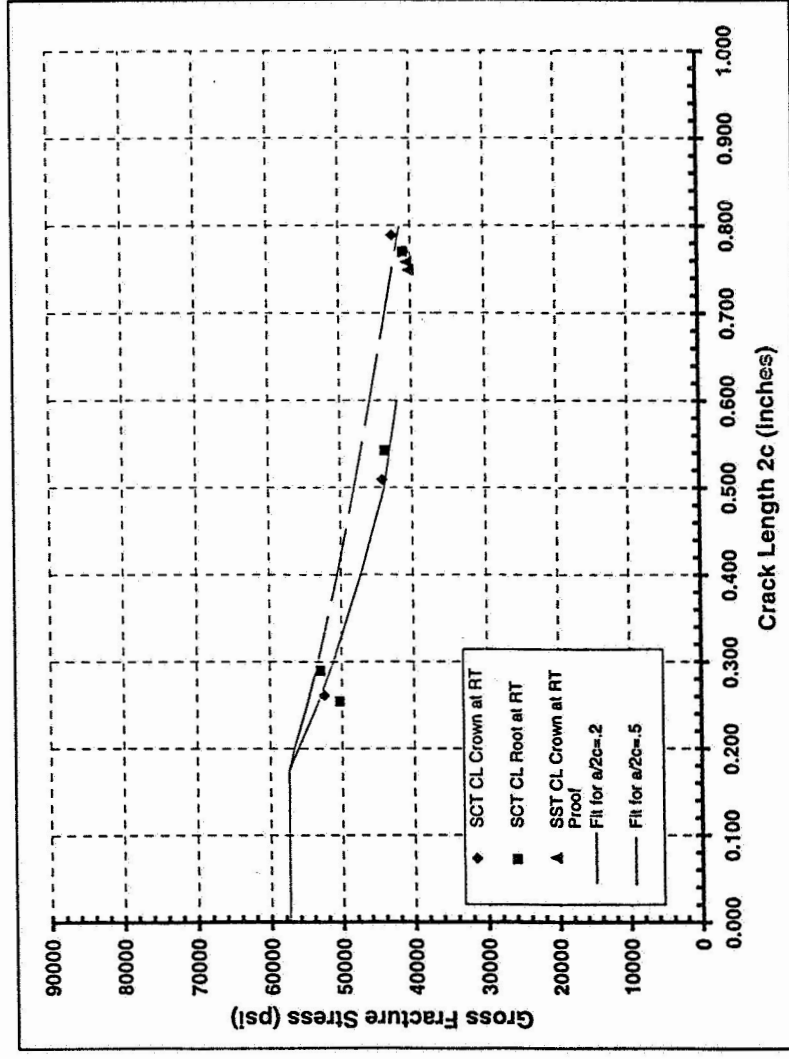
# FSWeld Surface Crack Tension Tests



a/2c Ratio	Target Flaw Size	
	a (in)	2c (in)
0.50	0.125	0.250
	0.250	0.500
0.20	0.150	0.750

- Tests conducted at RT, -320F and -423F
- Flaws oriented parallel to the weld direction and perpendicular to the load direction
- Initiated by EDM and increased to size under cyclic axial tension
- CL Crown and CL Root locations demonstrated lowest toughness
- LI and TI Root locations generated wide scatter in toughness data

# FSWeld SCT Gross Fracture Stress Results

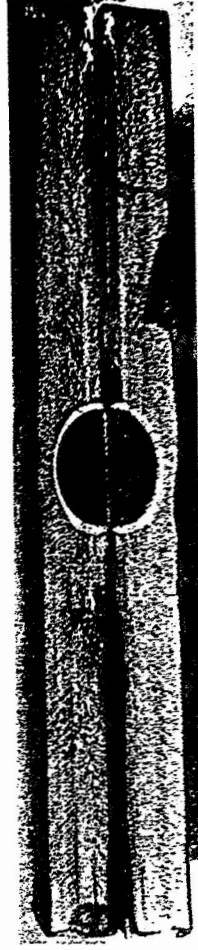


- CL flaw data plotted
- Limited data
- Threshold of 0.180" suggested ( $a/2c = 0.5$  and  $a/2c = 0.2$ )
- SST data included



**SCT at -320F with LI Root Flaw**

AeroMat 2000LOP MeclProp.ppt  
Rev Date: 04/12/2000



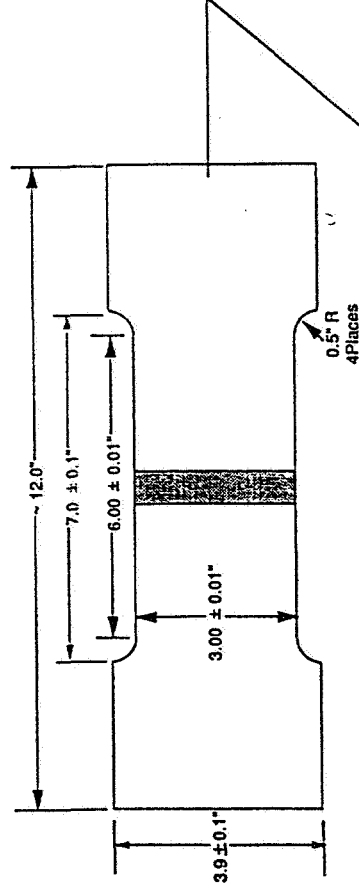
**SCT at -320F with CL Crown Flaw**

D. G. Kinchen (504)-257-1454  
E-Mail: david.kinchen@mat.nasa.gov

# FSWeld Simulated Service Tests

## Fracture Specimen

(Use NC Tape F-4)



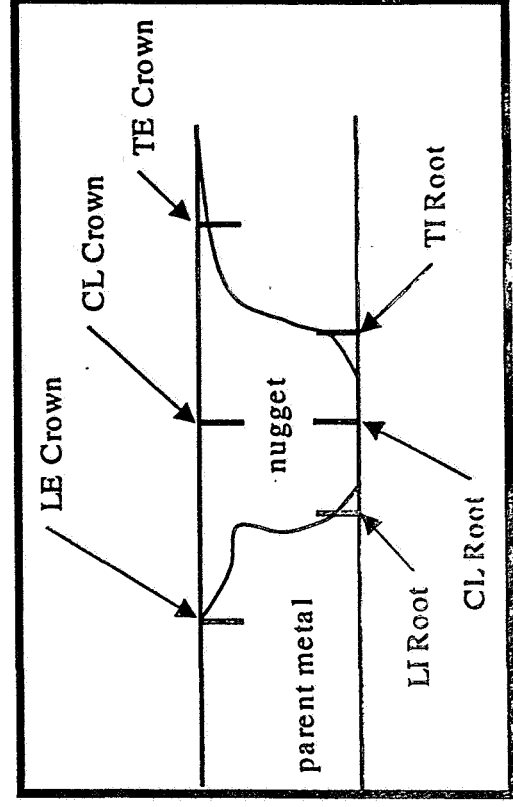
ID both ends with  
Sample no. shown on layout

### Note

Sawcut dimensions to be 4.0" x 12."

## Simulated Service Test Conditions

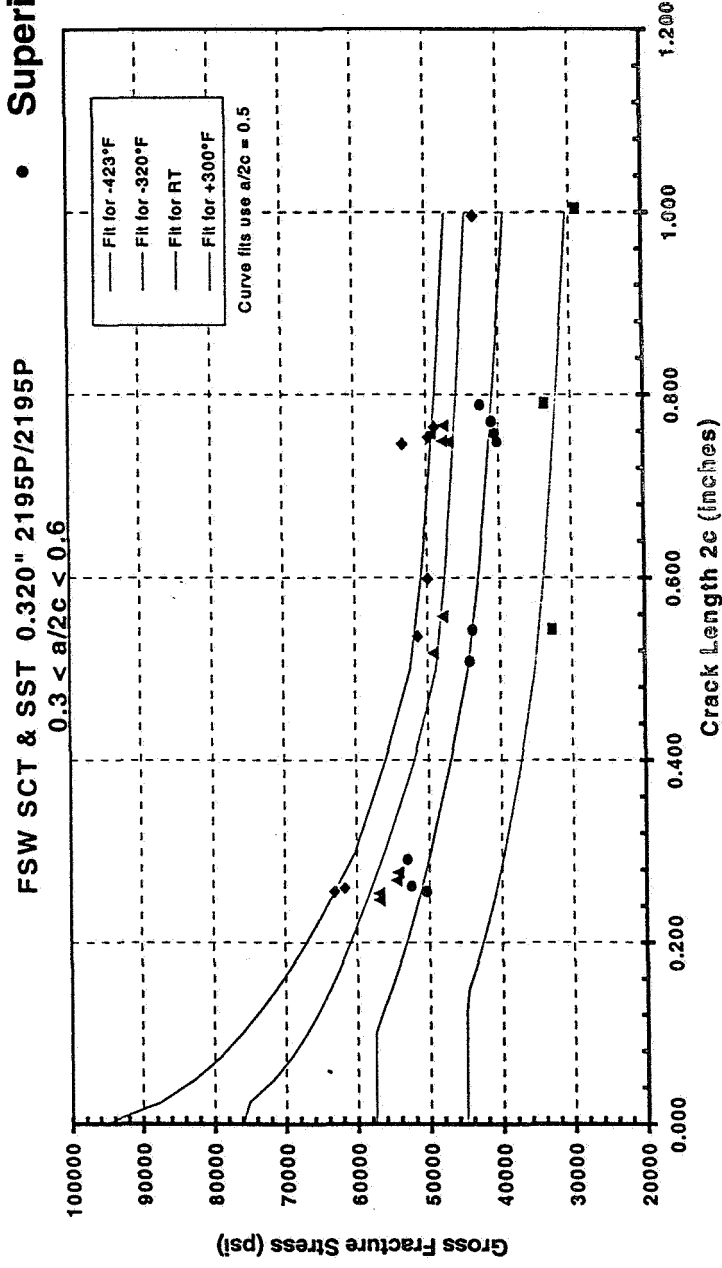
- Pre-cracked flaws and natural LOP
- Multiple flaw locations
- RT, -423°F & +300°F
- Multiple RT proof cycles, hold at specified stress, repeated for multiple mission simulation



# FSWeld Simulated Service Tests Results

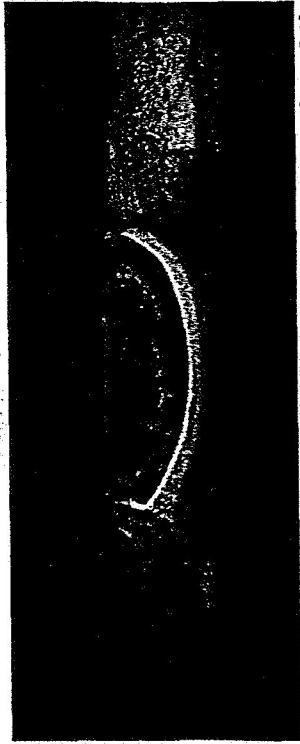
## • LOP - SST Results

- Consistent, repeatable results
- Predictable as a function of LOP depth
- Superior to fusion weld results



# FSWeld Simulated Service Tests Results

0.25 X 0.80" Flaw

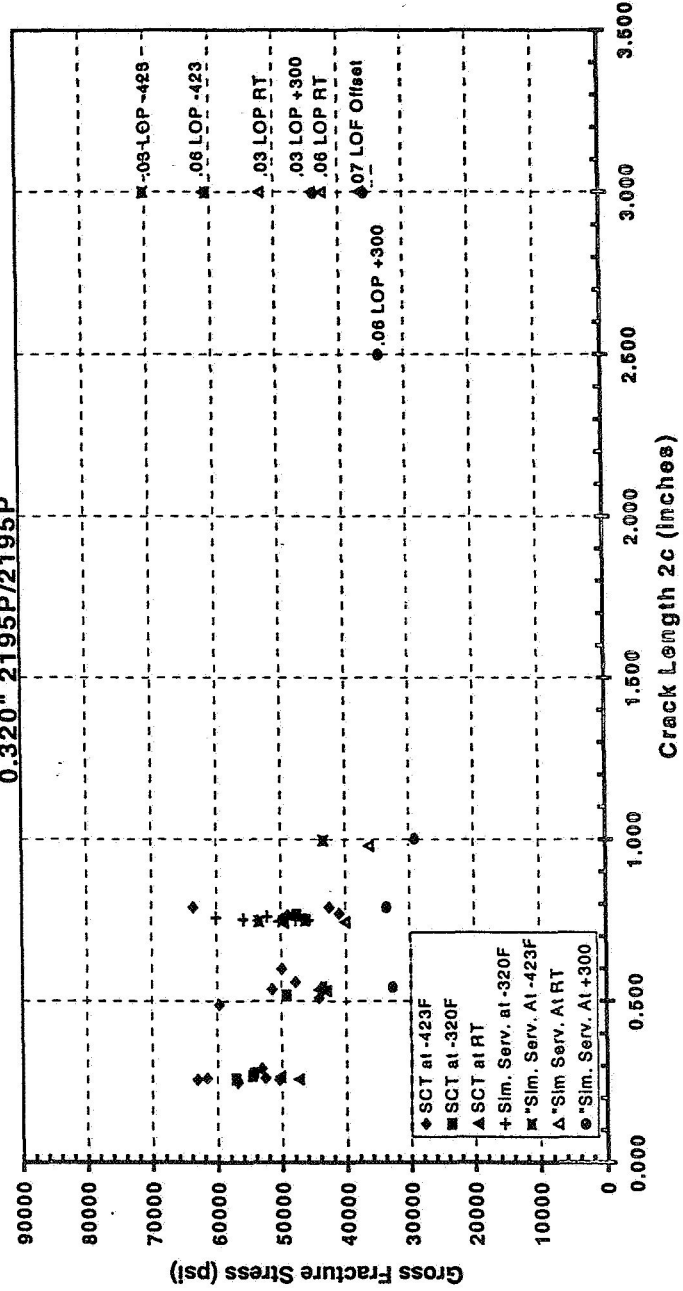


0.06" LOP



Friction Stir Weld SCT & SST Data

0.320" 2195P/2195P





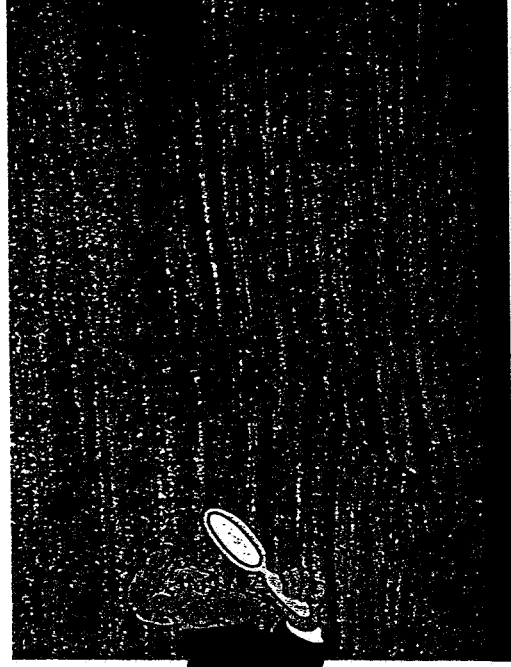
# FSWeld NDE Feasibility for LOP Inspection

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- ***Conventional Ultrasonics***

- Contact & Immersion
- 0, 45 and 60° Transducers
- Shear wave
- Creeping wave
- Dual Element
- Sonic Systems/Automated Inspection Systems
- Krautkramer



- ***Conventional Eddy Current***

- Zetec

- ***High Sensitivity Eddy Current***

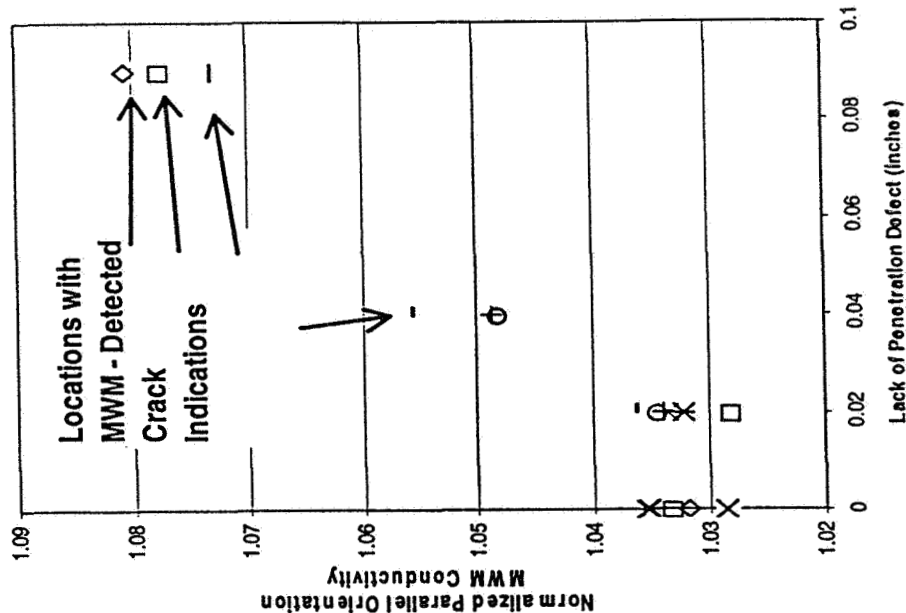
- MWM sensor
- Jentek Sensors

- ***Phased Array UT***

- 64 element array
- Shear wave
- R/D Tech

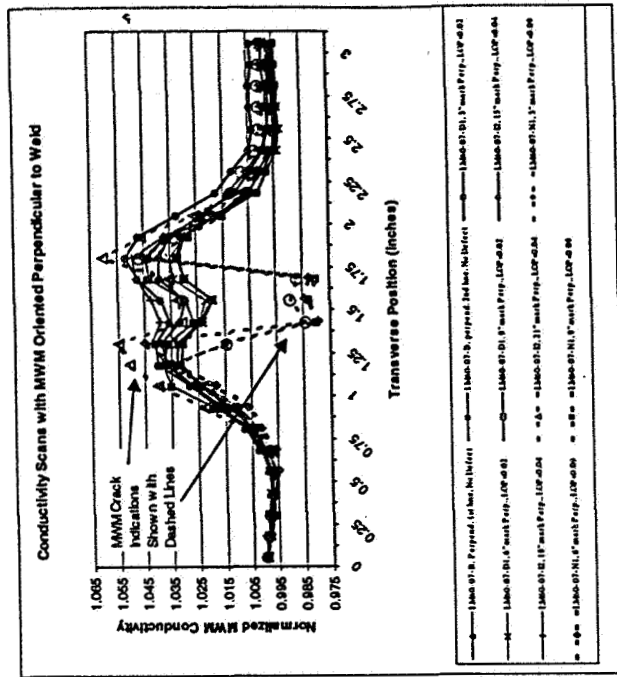
# FSWeld NDE Feasibility Results

## Minimum Center Region Normalized Conductivity



◊ IM60-07-B Parallel 1st line No Defect  
 ◊ IM60-07-B parallel 2nd line No Defect  
 ◊ IM60-07-D1 3" mark II LOP = 0.02  
 X IM60-07-D1 6" mark II LOP = 0.02  
 X IM60-07-D1 9" mark II LOP = 0.02  
 X IM60-07-D1 15" mark II LOP = 0.04  
 X IM60-07-D1 18" mark II LOP = 0.04  
 X IM60-07-D1 21" mark II LOP = 0.04  
 X IM60-07-N1 3" mark II LOP = 0.09  
 X IM60-07-N1 6" mark II LOP = 0.09  
 X IM60-07-N1 9" mark II LOP = 0.09  
 X IM60-07-A2 15" mark II No Defect  
 X IM60-07-A2 18" mark II No Defect  
 X IM60-07-A2 21" mark II No Defect  
 X IM60-07-E6 6" mark II LOP = 0.02  
 X IM60-07-E12 12" mark II LOP = 0.02  
 X IM60-07-E18 18" mark II LOP = 0.02

- **MWM Eddy Current**
  - Jentek Sensors, Inc.
  - 0.040" detected
  - Possibility of greater detectability



◊ IM60-07-B Prepared for test No Defect  
 ◊ IM60-07-B prepared for test No Defect  
 X IM60-07-D1 3" mark II LOP = 0.02  
 X IM60-07-D1 6" mark II LOP = 0.02  
 X IM60-07-D1 9" mark II LOP = 0.02  
 X IM60-07-D1 15" mark II LOP = 0.04  
 X IM60-07-D1 18" mark II LOP = 0.04  
 X IM60-07-D1 21" mark II LOP = 0.04  
 X IM60-07-N1 3" mark II LOP = 0.09  
 X IM60-07-N1 6" mark II LOP = 0.09  
 X IM60-07-N1 9" mark II LOP = 0.09  
 X IM60-07-A2 15" mark II No Defect  
 X IM60-07-A2 18" mark II No Defect  
 X IM60-07-A2 21" mark II No Defect  
 X IM60-07-E6 6" mark II LOP = 0.02  
 X IM60-07-E12 12" mark II LOP = 0.02  
 X IM60-07-E18 18" mark II LOP = 0.02

Figure 3: Normalized MWM Conductivity Scans for Friction Stir Weld Specimens, with MWM Oriented Perpendicular to Weld.

# FSWeld NDE Feasibility Results

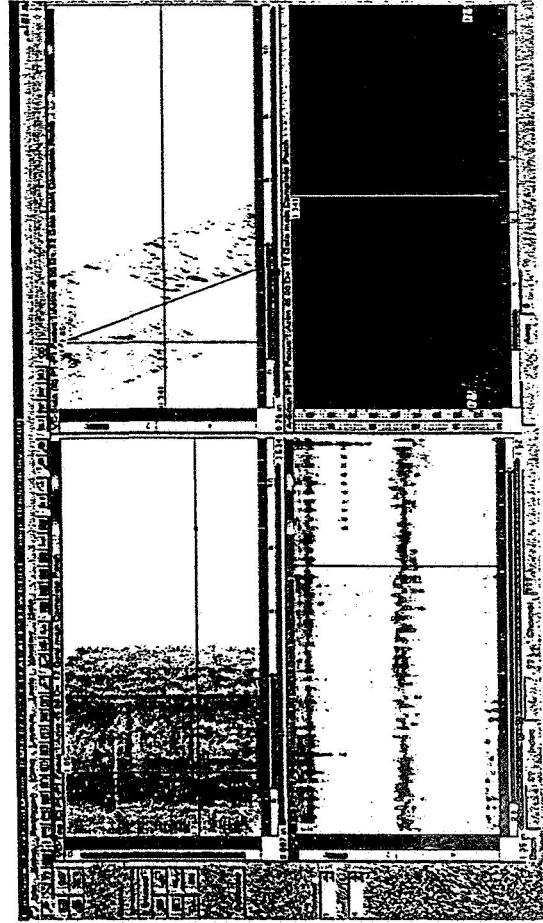
- *Phased Array UT*
  - R/D Tech Inc.
  - 0.060" LOP results shown
  - Possibility of greater detectability



# FSWeld NDE Feasibility Results

- *Phased Array UT*
  - LMSS Michoud Operations
  - 0.030" and 0.060" LOP detected post proof

0.03" deep LOP



0.06" Deep LOP



# Results

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- **Conventional Ultrasonics**

- **Sonic Systems/Automated Inspection Systems**

- Creeping wave and Dual Element FAST probes detected 0.040" LOP intermittently
- Easily detected deep LOP (0.090")

- **Krautkramer**

- Contact & Immersion 0, 45 and 60° Transducers, and Shear wave
- Readily detected 0.060" deep LOP

- **Conventional Eddy current**

- **Zetec**

- Readily detected 0.090" LOP, but not 0.040".
- Recommended development of other NDE methods



## Results

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- Mechanical property tests of FSW in 0.320" Al 2195 demonstrated an average RT UTS of 59 ksi, with a cryogenic enhancement factor of 1.5 and elongation of ~10%. All of these values are above those currently attainable with fusion weld processes. 0.650" Al 2195/Al 2219 FSWelds average RT UTS is 47 ksi with similar cryo enhancement and elongation.
- Lack Of Penetration is NOT an inherent condition in FSWelds of Al 2XXX alloys. Adequate process controls preclude LOP.
- SCT and SST tests of induced cracks resulted in gross fracture stress values above the values associated with current fusion weld processes.
- Tensile and fracture test results of LOP indications demonstrate predictable results well above comparable fusion welds at RT, cryogenic and elevated temperatures .
- Multiple NDE techniques exist or have shown feasibility to detect LOP in FSWelds.